

Inhibition and promotion of an isothermal flame in the low-pressure thermal decomposition of nitrogen trichloride

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The inhibition and promotion of an isothermal flame by NOCl and H₂, respectively, are considered based on a kinetic mechanism taking into account energy chain branching.

Previously, we reported the numerical simulation of some kinetic features of the branching chain process (BCP) of nitrogen trichloride (NCl₃)^{1–3} decomposition due to nonlinear steps in the BCP mechanism. Unlike hydrogen oxidation, which is a model BCP governed by linear chain branching, NCl₃ decomposition is controlled largely by the positive chain interaction (reaction in which the number of free valences increases as a result of the interaction of active centres⁴). This phenomenon gives rise to structural-organization effects, namely, isothermal flames^{5–8} and chemical oscillations.⁹ The experimental data on self-ignition, oscillating regimes, velocities and limits of isothermal flame propagation (IFP) in various diluents and a transition from IFP to a chain-thermal flame propagation were examined^{1–3} on the basis of a kinetic mechanism including energy chain branching.^{5,6} In all cases, the experimental and calculated data were in qualitative agreement. The region of IFP is much broader than the autoignition region.⁴ Therefore, because of the high fire hazard, special precautions should be taken in carrying out BCP with nonlinear steps. This is particularly true for industrially important reactions such as silane oxidation and electrolytic chlorine production, where NCl₃ is a by-product.^{10,11}

The branching chain mechanism, which means competition between chain branching and termination, is a crucial factor in gas-phase combustion between a few Torr and super atmospheric pressure.¹² Because the temperature rise, which accelerates branching chain reactions, results from this reaction, combustion can be effectively controlled by chemical means. In view of this, it is essential to develop flammability control methods for nonlinear BCP, in which a radical avalanche can form at a combustible-substance concentration below 1%.^{4,5} Thus, it is very important to study the inhibition and promotion of isothermal flames by active chemical additives. A study of NCl₃ decomposition in the presence of inhibitors and promoters is relevant to both explosion safety in chlorine industry and the

use of NCl₃ in laser chemistry.¹³

We consider the effects of inhibition and promotion on the IFP in dilute mixtures of NCl₃ in the presence of NOCl (inhibitor) or H₂ (promoter), taking into account the energy branching of chains.^{1–9} Earlier, we reported the inhibition of NCl₃ decomposition by NOCl⁸ and the promotion of this process by H₂.^{6,14} The possibility of inhibiting IFP was considered in terms of a generalised kinetic scheme.¹⁵

The experimental procedure was described elsewhere.^{3,5,6} Self-ignition limits were determined in a heated quartz reactor 20 cm in length and 6 cm in diameter. The inner surface of the reactor was covered with MgO, which provides the diffusive area of chain termination.⁸ To study inhibition, pure NOCl was admitted into a heated prepumped reactor. Next, an NCl₃–He mixture was added, and the reactor was allowed to stand for 5 min for perfect mixing. In promotion experiments, nitrogen trichloride was evaporated into hydrogen.

Figure 1 illustrates experimental data on the inhibition of IFP in NCl₃ by NOCl. As the inhibitor concentration is increased, the maximum flame velocity U decreases, the lower IFP limit rises, and the upper IFP limit decreases. It is noteworthy that the U value at the upper IFP limit is virtually independent of the inhibitor concentration at a constant NCl₃ concentration. Figure 2(a) presents experimental data illustrating the promotion of the IFP of 0.5% NCl₃ in H₂. For comparison, Figure 2(b) shows experimental flame velocity for helium containing 0.4 or 0.11% NCl₃.² A specific feature of the pressure dependence of the flame velocity in H₂ [Figure 2(a)] is that the upper IFP limit is not observed up to 500 Torr. The ratio between the diffusion coefficients of a probe particle in helium and hydrogen is ~0.9.¹⁶ The velocity of an isothermal flame is approximately equal to the square root of the diffusion coefficient of the active centre involved in positive chain interaction.⁴ It is clear from Figure 2 that, throughout the pressure range examined, the flame velocities in He and H₂ differ by a factor greater than 0.9^{1/2}.

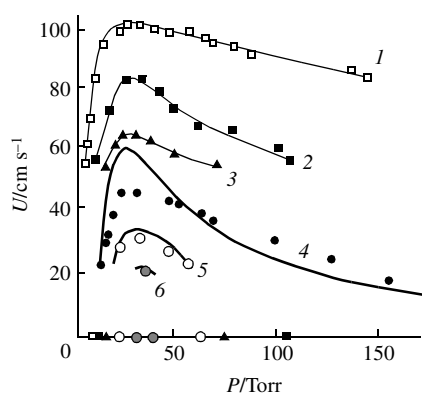


Figure 1 Flame velocity in NCl₃–He mixtures (1), (4) in the absence and (2), (3), (5), (6) in the presence of NOCl as a function of total pressure. [NCl₃] = (1)–(3) 0.8 and (4)–(6) 0.23%; [NOCl] = (1), (4) 0, (2) 0.024, (3) 0.041, (5) 0.02, and (6) 0.025%. The points represent experimental data; the thick solid lines show data calculated for model (I); and the thin solid lines are least-squares fits to experimental data.

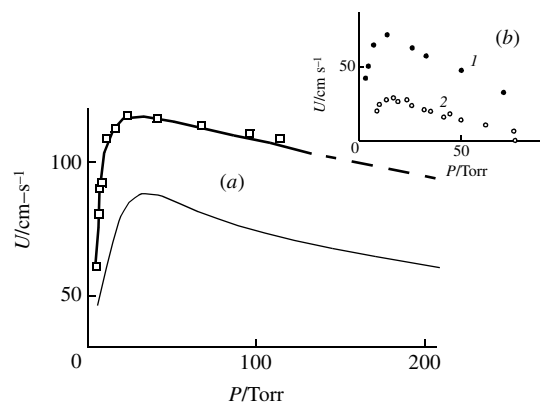


Figure 2 Flame velocity as a function of total pressure: (a) NCl₃ (0.5%)–H₂ mixture (the points represent experimental data;⁶ the thick line shows data calculated with allowance made for promotion; the thin line represents data calculated with allowance made for H₂ raising the diffusion coefficients of the intermediates without promoting NCl₃ decomposition) and (b) NCl₃–He mixture with [NCl₃] = (1) 0.4 and (2) 0.11%.⁶

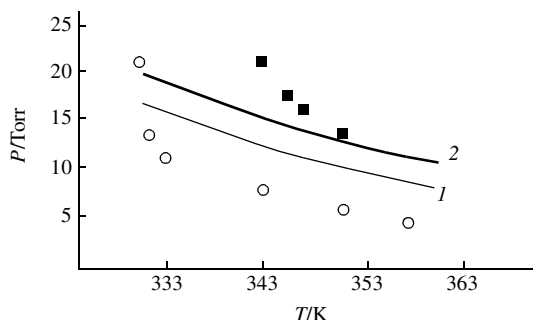
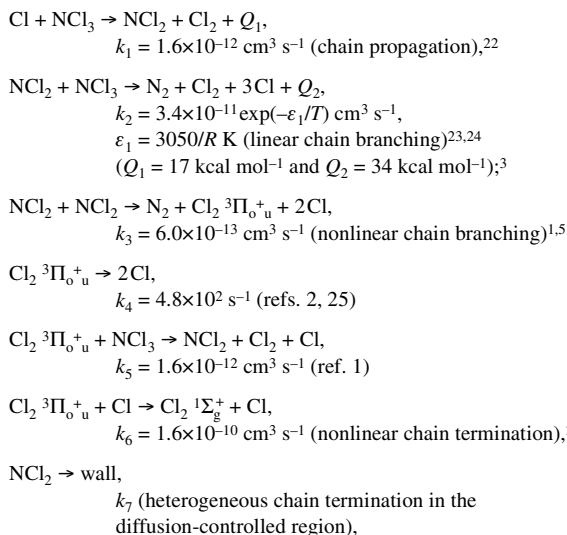


Figure 3 Temperature dependence of the lower autoignition limit for (1) NCl_3 (0.5%)– H_2 and (2) NCl_3 (0.4%)– He mixtures. The points and lines represent experimental and calculated data, respectively.

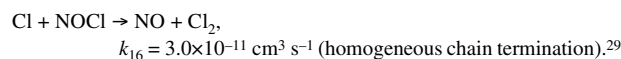
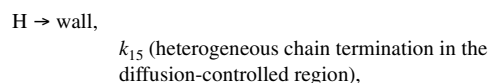
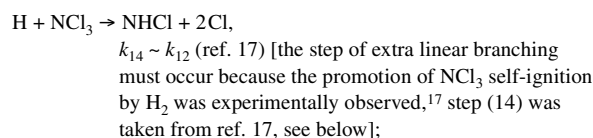
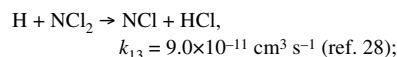
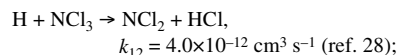
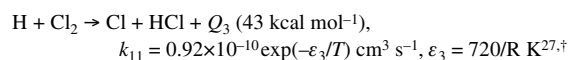
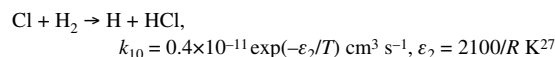
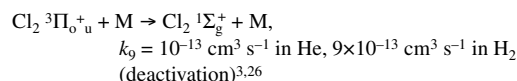
Figure 3 shows experimental flammability limits for NCl_3 – He and NCl_3 – H_2 mixtures. Flame propagation in the NCl_3 (0.5%)– H_2 mixture occurs outside the self-ignition region; that is, the flame observed in this mixture is isothermal (the measured temperature rise does not exceed a few Kelvins¹⁴). Note that the lower self-ignition limit P_1 for H_2 is lower than that for He . The reverse situation would be observed without a promoting effect because heterogeneous chain termination takes place in the diffusion-controlled region of chain termination, and the diffusion coefficient of a probe particle in H_2 is higher than that in He . Therefore, H_2 promotes NCl_3 decomposition in both autoignition¹⁷ and IFP regions. Raising the NCl_3 concentration in He widens the pressure range in which IFP is observed [Figure 2(b)]. We will demonstrate that, at the upper flame-propagation limit (0.4% NCl_3 , 70 Torr), the temperature rise ΔT is insufficient for self-ignition. The minimum self-ignition temperature is 333 K (Figure 3). Therefore, if the mixture is initially at 293 K, the minimum temperature rise ΔT_{\min} must be greater than 40 K. Let us refer to the relationship $\Delta T = QsP \times 3 \times 10^{16} / (C_p \rho N)$,¹⁸ where $C_p = 1.25 \text{ cal g}^{-1} \text{ K}^{-1}$ is the molar heat capacity of the NCl_3 – He mixture,¹⁹ P is the total pressure (Torr), s is the mole fraction of NCl_3 in the initial mixture ($[\text{NCl}_3]_0 = sP$), $N = 6.02 \times 10^{23} \text{ mol}^{-1}$, $\rho = 1.8 \times 10^{-4} \text{ g cm}^{-3}$ is the density of helium at 760 Torr,¹⁹ and $Q = 60 \text{ kcal mol}^{-1}$ is the heat of the reaction $\text{NCl}_3 \rightarrow 1/2 \text{N}_2 + 3/2 \text{Cl}_2$.²⁰ Hence, $\Delta T \sim 5 \text{ K} < \Delta T_{\min}$. This means that the upper flame-propagation limit is isothermal. The data calculated below are consistent with this inference. The chain-thermal flame propagation is clearly observed in H_2 containing 8% NCl_3 . In this case, flame propagates along the reactor with an apparent velocity of 400 m s^{-1} at 30 Torr and produces a characteristic sound.

Let us analyse experimental data on the IFP in terms of the known elementary reactions involved in NCl_3 decomposition. The kinetic mechanism of NCl_3 decomposition, including the steps occurring in the presence of H_2 (promoter) and NOCl (inhibitor), can be represented as follows;^{1–3,5,6,8,9,17,21,22}



$\text{Cl} \rightarrow \text{wall},$

k_8 (heterogeneous chain termination in the diffusion-controlled region),



We assumed that heat resulted from reactions (1), (2) and (11). The following equation corresponds to a heat balance:¹⁸

$$q_0 = (Q_1[\text{Cl}][\text{NCl}_3]k_1 + Q_2[\text{NCl}_2][\text{NCl}_3]k_2 + Q_3[\text{H}][\text{Cl}_2]k_{11}) / (C_p \rho) - \alpha L(T - 298) / (C_p \rho), \quad (1)$$

where Q_1 and Q_2 are the specific heats, C_p is heat capacity ($C_p = 1.25$ and $2 \text{ cal g}^{-1} \text{ K}^{-1}$ for the NCl_3 – He and NCl_3 – H_2 mixtures, respectively¹⁹), α is the heat-transfer coefficient, and L is the surface area-to-volume ratio (cm^{-1}). α was estimated³ from the relationship $\alpha = L\delta\lambda e/r^2$, where r is the reactor radius (cm), e is the Napierian base, $\delta = 2.0$ is the critical parameter, and λ is the heat conductivity of the mixture (which was taken equal to that of He in inhibition experiments and to that of hydrogen in promotion).

The problem is considered in a one-dimensional approximation. The characteristic scales of time, length and velocity, as well as dimensionless variables and parameters, were chosen as described previously:^{2,3}

$$\begin{aligned} \tau &= k_1[\text{NCl}_3]_0 t, & Y_0 &= [\text{Cl}]/[\text{NCl}_3]_0, & Y_1 &= [\text{Cl}_2 + 3\text{H}_2]/[\text{NCl}_3]_0, \\ Y_2 &= [\text{NCl}_2]/[\text{NCl}_3]_0, & Y_3 &= [\text{NCl}]/[\text{NCl}_3]_0, & \beta &= k_2/k_1, \\ \phi &= k_3/k_1, & \gamma &= k_8/(k_1[\text{NCl}_3]_0), & \lambda &= k_4/(k_1[\text{NCl}_3]_0), \\ \psi &= k_5/k_1, & \rho &= k_7/(k_1[\text{NCl}_3]_0), & \mu &= k_6/k_1, \\ \chi &= k_9/(k_1[\text{NCl}_3]_0). \end{aligned}$$

t is time (s), the dimensionless velocity and coordinate of the propagating flame were defined in terms of the diffusivity of NCl_3 (D_3): $\varpi = U/(D_3 k_1[\text{NCl}_3]_0)^{1/2}$, $\xi = x/(D_3 k_1[\text{NCl}_3]_0)^{1/2}$, where U and x are the corresponding dimensional values. Let us define the dimensionless diffusion coefficients of chlorine atoms – D_0 , $\text{Cl}_2 + 3\text{H}_2$ – D_1 , NCl_2 – D_2 , H atoms – D_5 , NOCl – D_6 , Cl_2 – D_7 , as δ_0 , δ_1 , δ_2 , δ_5 , δ_6 and δ_7 , respectively. Additional variables were introduced:

$$\begin{aligned} Y_5 &= [\text{H}]/[\text{NCl}_3]_0, & Y_6 &= [\text{NOCl}]/[\text{NCl}_3]_0, & Y_7 &= [\text{Cl}_2]/[\text{NCl}_3]_0, \\ \eta &= k_7/(k_1[\text{NCl}_3]_0), & \gamma &= k_8/(k_1[\text{NCl}_3]_0), & k &= k_{10}/k_1, \\ \pi &= k_{11}/k_1, & \theta &= k_{12}/k_1, & \zeta &= k_{13}/k_1, \\ \nu &= k_{15}/(k_1[\text{NCl}_3]_0), & \sigma &= k_{16}/k_1. \end{aligned}$$

Note that Y_4 is temperature (K). The mole fraction of NOCl in the mixture will be designated as v . Dimensionless thermal diffusivity is $\delta_4 = D/D_3$, where D is dimensional thermal diffusivity, which was taken equal to the self-diffusion coefficient of He ($1.62 \text{ cm}^2 \text{ s}^{-1}$ under normal conditions¹⁹).

Thus, we arrive at the following set of second-order partial differential diffusion-kinetic equations:

[†] The reverse of step (10) does not affect the calculated data.

$$\begin{aligned}
\partial Y_0/\partial \tau &= \delta_0 \partial^2 Y_0/\partial \xi^2 + 2\phi(Y_2)^2 + \psi Y_1 Y_3 + 2\lambda Y_1 - Y_0 Y_3 + \\
&\quad + 3Y_2 Y_3 \beta \exp(-\varepsilon_1/Y_4) - \kappa Y_0 \exp(-\varepsilon_2/Y_4)/s + 2\theta Y_3 Y_5 - \\
&\quad - \sigma Y_0 Y_6 v/s - \gamma Y_0 \\
\partial Y_1/\partial \tau &= \delta_1 \partial^2 Y_1/\partial \xi^2 + 2\phi(Y_2)^2 - \psi Y_1 Y_3 - \lambda Y_1 - \chi P Y_1 - \mu Y_0 Y_1 \quad (I) \\
\partial Y_2/\partial \tau &= \delta_2 \partial^2 Y_2/\partial \xi^2 - 2\phi(Y_2)^2 + \psi Y_1 Y_3 - \eta Y_2 - Y_2 Y_3 \beta \exp(-\varepsilon_1/Y_4) + \\
&\quad + \theta Y_3 Y_5 - \zeta Y_2 Y_5 + Y_0 Y_3 \\
\partial Y_3/\partial \tau &= \delta_3 \partial^2 Y_3/\partial \xi^2 - \psi Y_1 Y_3 - Y_0 Y_3 - Y_2 Y_3 \beta \exp(-\varepsilon_1/Y_4) - 2\theta Y_3 Y_5 \\
\partial Y_4/\partial \tau &= \delta_4 \partial^2 Y_4/\partial \xi^2 + 3.8 \times 10^{-5} s [Q_2 Y_2 Y_3 \beta \exp(-\varepsilon_1/Y_4) + \\
&\quad + Q_3 \pi Y_3 Y_7 \exp(-\varepsilon_3/Y_4) + Q_1 Y_0 Y_3]/(C_p \rho) - \\
&\quad - 10^{-6} (Y_4 - 298)/(s C_p \rho P^2) \\
\partial Y_5/\partial \tau &= \delta_5 \partial^2 Y_5/\partial \xi^2 - 2\theta Y_3 Y_5 + \kappa Y_0 \exp(-\varepsilon_2/Y_4)/s - \nu Y_5 - \zeta Y_2 Y_5 \\
\partial Y_6/\partial \tau &= \delta_6 \partial^2 Y_6/\partial \xi^2 - \sigma Y_0 Y_6 v/s \\
\partial Y_7/\partial \tau &= \delta_7 \partial^2 Y_7/\partial \xi^2 + \mu Y_0 Y_1 + \psi Y_1 Y_3 + 2\lambda Y_1 + Y_0 Y_3 + \chi P Y_1 + \\
&\quad + Y_2 Y_3 \beta \exp(-\varepsilon_1/Y_4) - \pi Y_0 \exp(-\varepsilon_3/Y_4)
\end{aligned}$$

The solutions to set (I) satisfy the following boundary conditions for flame propagating from the right to the left:^{2,3}

$$\begin{aligned}
Y_0, Y_1, Y_2, Y_4, Y_5 &\rightarrow 0, \xi \rightarrow \pm\infty \\
Y_3 &\rightarrow 1, \xi \rightarrow -\infty; \quad Y_3 \rightarrow 0, \xi \rightarrow +\infty; \quad Y_6 \rightarrow v/s, \xi \rightarrow -\infty.
\end{aligned} \quad (II)$$

The chain-initiation reaction is ignored.¹⁵ Based on experimental data, we simulated the inhibition of an isothermal flame and flame promotion (in the former case, the reactions involving H and H₂ were excluded from set (I); in the latter case, the reactions involving NOCl were excluded). The set of equations (I) was solved numerically.³ Since heterogeneous chain termination was considered to occur in the diffusion-controlled region, the rate constants k_7 , k_8 and k_{14} were calculated³ using the D_i values of the reaction mixture components.^{3,16} The procedure for determining the autoignition limits is described below.³⁰ The deviation of concentration Y_1 from its stationary values can be expressed as $Y_1 - Y_{1st} = A_1 \exp \omega_1 t + A_2 \exp \omega_2 t + A_3 \exp \omega_3 t + A_4 \exp \omega_4 t$, where A_i are constants. Let this be true for the other Y_i . The exponents are defined by the eigenvalues of the following matrix (note that the elements of this matrix contain only terms corresponding to the reaction intermediates and to the elementary reactions that are linear with respect to these intermediates):

$$\begin{vmatrix}
\partial/\partial Y_0(dY_0/d\tau) - \omega & \partial/\partial Y_1(dY_0/d\tau) & \partial/\partial Y_3(dY_0/d\tau) & \partial/\partial Y_5(dY_0/d\tau) \\
\partial/\partial Y_0(dY_1/d\tau) & \partial/\partial Y_1(dY_1/d\tau) - \omega & \partial/\partial Y_3(dY_1/d\tau) & \partial/\partial Y_5(dY_1/d\tau) \\
\partial/\partial Y_0(dY_3/d\tau) & \partial/\partial Y_1(dY_3/d\tau) & \partial/\partial Y_3(dY_3/d\tau) - \omega & \partial/\partial Y_5(dY_3/d\tau) \\
\partial/\partial Y_0(dY_5/d\tau) & \partial/\partial Y_1(dY_5/d\tau) & \partial/\partial Y_3(dY_5/d\tau) & \partial/\partial Y_5(dY_5/d\tau) - \omega
\end{vmatrix} = 0 \quad (2)$$

Matrix (2) is equivalent to the equation $\omega^4 + A\omega^3 + B\omega^2 + C\omega + D = 0$. Coefficients A , B , and C have a constant sign for the above kinetic scheme. Coefficient D , which is the determinant of matrix (2), changes its sign. When this happens, at least one of the exponents infinitely grows, implying ignition. By equating determinant (2) to zero, we define a curve that is a boundary of the autoignition region on the (P, T) plane. Because termolecular chain termination was ignored in our calculations,² we determined only the lower autoignition limit. Figure 1 presents the results of a numerical simulation of the inhibition of IFP (thick lines). These results were obtained for $k_{16} = 1.4 \times 10^{-11} \text{ cm}^3 \text{ s}^{-1}$. We can judge only qualitative agreement between the calculated and observed data. It was not our aim to fit the calculated flame velocities and IFP limits to experimental data by varying constants k_i . This fitting would be of a low value because a large number of parameters would be introduced in the calculation. This is also true of step (14); the establishment of the chemical nature of the extra linear branching step calls for further investigation. However, the observed decrease in the flame velocity and the narrowing of the IFP region, caused by an increase in the inhibitor concentration in a combustible mixture, is qualitatively predicted by set (I). Figure 2(a) presents calculated data that illustrate the promotion of an IFP flame. A comparison between the calculated and experimental data confirms that flame propagation in the 0.5% NCl₃ + H₂ mixture is isothermal. Both

experiments and calculations suggest that IFP occurs outside the autoignition region (see above). Furthermore, calculated data [Figure 2(a), thin line] demonstrate that raising the diffusion coefficients of the intermediates in H₂ without allowing for promotion will not fit the calculated data to the observed data. Therefore, the IFP velocity in H₂ is higher than that in He owing to H₂ promoting NCl₃ decomposition [Figure 2(b)]. As demonstrated for the reaction between NCl₃ and H₂ near the lower autoignition limit,¹⁷ reaction (10) is a link between NCl₃ decomposition and additional branching reaction (14) (promotion).

Thus, we analysed experimental data on the inhibition and promotion of IFP for NCl₃ decomposition in helium in the presence of NOCl (inhibitor) and H₂ (promoter). We performed a numerical simulation of this process taking into account energy chain branching. The results are in qualitative agreement with experimental data. Based on previous data^{1–3} and this work, the reaction near the lower self-ignition limit can be considered as a model nonlinear BCP.

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